

P.O. Box 27 • Helena, Montana 59624 Tel: (406) 457-0407 • Fax: (406) 442-1296 www.bigskyacoustics.com



November 12, 2019

Mr. Chris Cote MDT Environmental Services PO Box 201001 Helena MT 59620-1001

Re: Rumble Strip Wayside Noise Study Experimental Project MT-18-02, UPN 9370000 BSA Project #19134

Dear Chris:

Big Sky Acoustics (BSA) has completed MDT's Rumble Strip Wayside Noise Study project. The attached report summarizes the field methodology, measurement results and recommendations, and incorporates MDT's comments received on the draft report.

Thank you for the opportunity to work with MDT on this experimental project. If you have any questions concerning this report, please do not hesitate to call me at (406) 457-0407, or email me at sean@bigskyacoustics.com.

Sincerely,

Jem Comoly

Sean Connolly, INCE Bd. Cert. BIG SKY ACOUSTICS

Attachment

cc: Joe Radonich/MDT Craig Abernathy/MDT

RUMBLE STRIP WAYSIDE NOISE STUDY EXPERIMENTAL PROJECT MT-18-02, UPN 9370000





Completed by:



TABLE OF CONTENTS

Section	n Page
1.0	BACKGROUND, PURPOSE & STUDY DESIGN1
2.0	NOISE TERMINOLOGY1
3.0	FIELD METHODOLOGY23.1EQUIPMENT.3.2WAYSIDE NOISE LEVEL MEASUREMENTS.3
4.0	RESULTS
5.0	LITERATURE REVIEW10
6.0	CONCLUSIONS11
7.0	RECOMMENDATIONS
8.0	REFERENCES
TADI	FS

TABLES

TABLE 2-1	CHANGES IN NOISE LEVELS VS. APPARENT CHANGE IN LOUDNESS
TABLE 3-1	WEATHER DATA RECORDED DURING MEASUREMENTS
$T \cdot p \cdot p \cdot q \cdot 1$	DEPENDENCE OF OCL DO NOVER LEVELS TO THE OLDO AND DAVED OF

- TABLE 4-1
 DIFFERENCE OF SCLRS NOISE LEVELS TO THE CLRS AND PAVEMENT
- TABLE 4-3
 DRIVER INTERIOR OBSERVATIONS NOTED DURING TESTING

FIGURES

FIGURE	1	RUMBLE ST	RIP SECTION	ons and N	IOISE	LEVEL	MEASURE	EMENT LOCA	TIONS
				-	-		-	-	

- $FIGURE \ 4-1 \qquad Measured \ Average \ Overall \ L_{max} \ Noise \ Levels \ --Passenger \ Vehicle$
- $FIGURE \ 4-2 \qquad Measured \ Average \ Overall \ L_{max} \ Noise \ Levels \ --Medium \ Truck$
- FIGURE 4-3 MEASURED AVERAGE OVERALL L_{MAX} NOISE LEVELS—HEAVY TRUCK
- FIGURE 4-4 MEASURED AVERAGE LMAX 1/3-OCTAVE BAND FREQUENCY SPECTRA
- FIGURE 6-1 DIFFERENCE BETWEEN CLRS AND SCLRS NOISE LEVELS—PASSENGER VEHICLE
- FIGURE 6-2 DIFFERENCE BETWEEN CLRS AND SCLRS NOISE LEVELS—MEDIUM TRUCK
- FIGURE 6-3 DIFFERENCE BETWEEN CLRS AND SCLRS NOISE LEVELS—HEAVY TRUCK

APPENDICES

APPENDIX A PHOTO LOG APPENDIX B FIELD NOTES

ACRONYM LIST

dBdecibelsdBAA-weighted decibelsCaltransCalifornia Department of Transportation
dBA A-weighted decibels California Department of Transportation
Caltrans California Department of Transportation
Canualis Camorina Department of Transportation
CLRS centerline rumble strip
FHWA Federal Highway Administration
Hz hertz
L _{max} maximum instantaneous sound level
MDT Montana Department of Transportation
MNDOT Minnesota Department of Transportation
mph miles per hour
MWHC Mountain West Holding Company
NCHRP National Cooperative Highway Research Program
RP reference post
SCLRS sinusoidal centerline rumble strip
TRB Transportation Research Board
WSDOT Washington State Department of Transportation

1.0 BACKGROUND, PURPOSE & STUDY DESIGN

The Montana Department of Transportation (MDT) initiated the Rumble Strip Wayside Noise Study to determine if sinusoidal rumble strips result in lower exterior noise levels at noise sensitive locations, such as residences, located adjacent to Montana roadways. Rumble strips are an effective traffic safety feature, but have caused increased citizen complaints in the last decade due to noise when vehicle tires strike MDT's standard rumble strip.

Big Sky Acoustics (BSA) teamed with Mountain West Holding Company (MWHC) to complete this project. This wayside noise study helped determine whether or not a particular design of sinusoidal centerline rumble strips (SCLRS) reduced exterior noise compared to MDT's standard centerline rumble strip (CLRS).

In 2018, a contractor installed four test sections of milled (i.e., in-ground) SCLRS on MT-39 (P-39N) between Reference Post (RP) 31 and RP 32.4, approximately 8 miles north of Colstrip, Montana. MDT's standard CLRS is located at both ends of the sinusoidal rumble strips. The sections tested for this wayside noise study included the following, and are documented in the photolog in **Appendix A**:

- 1. Standard 12" wide CLRS, ¹/₂" to 5/8" depth, milled in pairs, 36" on center
- 2. SCLRS Design S1: 14" longitudinal frequency, 12" wide, 1/8" to 1/2" depth
- 3. SCLRS Design S2: 24" longitudinal frequency, 12" wide, 1/8" to ½" depth
- 4. SCLRS Design S3: 14" longitudinal frequency, 14" wide tapered, 1/8" to 1/2" depth
- 5. SCLRS Design S3A: 24" longitudinal frequency, 14" wide tapered, 1/8" to 1/2" depth
- 6. Chipseal Pavement (Type 1, 3/8" aggregate) without striking the rumble strip (i.e., baseline).

The SCLRS installation and details are provided in MDT's *Sinusoidal Centerline Rumble Strip Evaluation* report (MDT 2019). The rumble strip sections are shown on **Figure 1** (attached).

2.0 NOISE TERMINOLOGY

Noise levels are quantified using units of decibels (dB). The L_{max} metric denotes the maximum instantaneous sound level recorded during a measurement period. Humans typically have reduced hearing sensitivity at low frequencies compared with their response at high frequencies. The "A-weighting" of noise levels, or A-weighted decibels (dBA), closely correlates to the frequency response of normal human hearing (250 to 4,000 hertz [Hz]).

Noise levels typically decrease by approximately 6 dBA every time the distance between the source and receptor is doubled, depending on the characteristics of the source and the conditions over the path that the noise travels. The reduction in noise levels can be increased if a solid barrier or natural topography blocks the line of sight between the source and receptor.

Since a person's response to noise is subjective, the perception of noise can vary from person to person. **Table 2-1**, on the following page, indicates the relationship between changes in noise levels and a person's typical perception of the change.

Change in Sound Level (dBA)	Apparent Change in Loudness to a Person	
±1	Imperceptible	
±3	Barely audible (i.e., barely noticeable reduction)	
±5	Clearly audible (i.e., clearly noticeable reduction)	
±10	Half as loud or twice as loud as the original noise (significant change)	
±20	One quarter as loud or four times as loud as the original noise (very significant change)	

Table 2-1: Changes	in Noise	Levels vs.	Apparent	Change in	Loudness
Tuble - It Changes			i ippui chi	Chunge in	Loudicos

Source: Egan 1988

3.0 FIELD METHODOLOGY

Fieldwork was completed on July 29-30, 2019. On July 29, the Team met in Billings and discussed traffic control, communication, equipment, and measurement specifics. Using information in MDT's SCLRS report and field observations, BSA also identified, measured and flagged the noise measurement and vehicle strike locations along MT-39, and ensured the ground conditions and topography at each of centerline rumble strip measurement locations were similar (**Appendix A**).

Early morning on July 30, MWHC set up the traffic control signage and cones for the 2-lane, shortterm flagging operation on MT-39, which included all residential approaches and private roads. The Team conducted a safety and coordination meeting prior to the testing, and was in continuous radio-communication during the fieldwork. The team consisted of a noise specialist (BSA), passenger vehicle driver (BSA), medium truck driver (MWHC), heavy truck driver (MWHC), traffic control supervisor (MWHC), and two flaggers (MWHC). MDT provided oversight of the field operations.

The standard CLRS, the four SCLRS designs, and the existing chipseal pavement were tested separately. For each measurement location, the strike zones were marked by cones on both shoulders and a clear view of the road was visible over relatively flat ground for several hundred feet in each direction (**Appendix A**). The vehicles drove over the rumble strips with the tires closest to the sound level meter (SLM) so that the vehicles did not shield the equipment. Depending on traffic control, some tests were conducted in both north/south directions and some tests were conducted one-way. Traffic was not held or delayed more than 10 minutes at a time during the fieldwork. Testing proceeded from south to north, and the measurement locations and rumble strip sections are shown on **Figure 1**.

The three test vehicles (passenger vehicle, medium truck and heavy truck) passed by the SLM while striking the rumble strip for a minimum of 100 feet on each side of the measurement location (200 feet total). Three measurements were completed for each vehicle passing by the SLM measurement location at each of the test speeds (30, 50 and 70 mph), three times each, at the six sections (Section 1.0).

3.1 Equipment

As shown in the photolog in Appendix A, the vehicles used for the tests included the following:

- 1. Passenger vehicle (2-axle, 4-tire): 2018 Toyota 4Runner, P265/70R17 (10.4-inch tire width)
- 2. Medium truck (2-axle, 6-tire): 2007 Dodge Ram 3500 Dually, P230/80R17 (9-inch tire width)
- 3. Heavy truck: (3-axle, 10-tire): 2000 Volvo Truck Tractor, P275/11R22.5 (10.8-inch tire width)

BSA conducted the measurements with a Larson Davis Model 831 Type I SLM set to fast response, with a preamplifier and 0.5-inch diameter microphone. The meter was field-calibrated using a Larson Davis Model CAL200 prior to each measurement location, and verified at the conclusion of the measurements.

The SLM was located 50 feet from the centerline rumble strip at each test section, with a clear view of the roadway. For each measurement, the microphone was 5 feet above the road surface, which was between 8- and 9.5-feet above the ground surface at the measurement locations as shown in **Appendix A**. A wind screen as used over the microphone.

3.2 Wayside Noise Level Measurements

BSA conducted the wayside noise level measurements in general accordance with AASHTO TP 98-18, *Standard Method of Test for Determining the Influence of Road Surfaces on Vehicle Noise Using the Statistical Isolated Pass-by Method*, and FHWA's *Measurement of Highway-Related Noise*. For each vehicle pass-by, the overall L_{max} noise levels and the 1/3 octave band frequency L_{max} spectra (50 to 10,000 Hz) were recorded, and the SLM recorded an audio clip for reference. The measurements were conducted between approximately 0725 and 1410 hours, and the field notes are included in **Appendix B**.

Temperature, relative humidity, wind speed/direction were measured using Kestrel 3000 meter. The data is shown in **Table 3-1**. The data indicates atmospheric conditions did not affect the measured sound levels, primarily because the wind speed throughout the measurements was calm to 3 mph.

Time (hours)	Temperature	Relative Humidity	Wind speed
0750	67°F	66%	Calm
0840	79°F	68%	Calm
0915	84°F	50%	Calm to 3 mph from S
0945	82°F	55%	Calm
1100	87°F	51%	Calm
1215	92°F	41%	Calm to 3 mph from S
1305	92°F	39%	Calm to 3 mph from S
1330	90°F	40%	Calm to 3 mph from S

 Table 3-1: Weather Data Recorded during Measurements

4.0 **RESULTS**

For comparison, the L_{max} of the measured sound level data from the three tests for each vehicle and speed combination were calculated and averaged. The 1/3-octave band frequency L_{max} measurement data for each vehicle tested are included in **Section 4.2**.

Although the goal of this project was to compare the wayside noise levels of the SCLRS designs, the wayside noise levels due to vehicles traveling on the chipseal pavement, without striking the rumble strips, were also field-measured. This baseline measured pavement data is included in the results shown in the following subsections for comparison to the SCLRS designs and standard CLRS.

4.1 Wayside Noise Level Results

4.1.1 Passenger Vehicle

The measured average overall L_{max} sound levels for the passenger vehicle are summarized on **Figure 4-1**. As shown, the wayside noise levels of the standard CLRS are the highest at each speed, but more notably at 50 and 70 mph. The wayside noise levels of the four SCLRS are similar to each other, and one design is not significantly quieter than another. Compared to the CLRS, the wayside SCLRS noise levels of the passenger vehicle are 1.8 to 4.4 dBA quieter at 30 mph (i.e., a barely to clearly noticeable reduction), 8.2 to 9.2 dBA quieter at 50 mph (i.e., a clearly noticeable reduction to half as loud), and 12.8 to 13.4 dBA quieter at 70 mph, which is typically perceived as half as loud (**Table 2-1**) (Egan 1988). The wayside noise levels of the four SCLRS designs are also similar to the chipsealed pavement (baseline) at each of the three test speeds (**Figure 4-1**).



Figure 4-1: Measured Average Overall Lmax Noise Levels—Passenger Vehicle

4.1.2 Medium Truck

The measured average overall L_{max} sound levels for the medium truck are summarized on **Figure 4-2**. As shown, the wayside noise levels of the standard CLRS are the highest at 50 and 70 mph. The wayside noise levels of the four SCLRS are similar to each other, and one design is not significantly quieter than another. Compared to the CLRS, the wayside SCLRS noise levels of the medium truck are within -0.8 to 0 dBA of the CLRS at 30 mph (i.e., imperceptible), 2.4 to 4.2 dBA quieter at 50 mph (i.e., a barely noticeable reduction), and 5.1 to 6.1 dBA quieter at 70 mph, (i.e., a clearly noticeable reduction) (**Table 2-1**) (Egan 1988). The medium truck wayside noise levels of the four SCLRS designs are also similar to the chipsealed pavement (baseline) at 30 and 70 mph (**Figure 4-2**). However, at 50 mph, the SCLRS designs had lower noise levels than the pavement. This difference appears to be due to the engine sounds of the truck, which produced a tone at 100 Hz during the pavement noise level measurements (**Section 4.2**).



Figure 4-2: Measured Average Overall Lmax Noise Levels—Medium Truck

4.1.3 Heavy Truck

The measured average overall L_{max} sound levels for the heavy truck are summarized on **Figure 4-3**. As shown, the wayside noise levels of the standard CLRS are the highest at 50 and 70 mph. The wayside noise levels of the four SCLRS are similar to each other and one design is not significantly quieter than another. Compared to the CLRS, the wayside SCLRS noise levels of the heavy truck are within -0.5 to 3.2 dBA of the CLRS at 30 mph (i.e., imperceptible), 1.8 to 4.6 dBA quieter at 50 mph (i.e., a barely noticeable reduction), and 8.4 to 9.5 dBA quieter at 70 mph, (i.e., a clearly noticeable reduction to half as loud) (**Table 2-1**) (Egan 1988). The heavy truck wayside

noise levels of the four SCLRS designs are also similar to the chipsealed pavement (baseline) at each of the three test speeds (**Figure 4-3**).



Figure 4-3: Measured Average Overall Lmax Noise Levels—Heavy Truck

4.2 Analysis

Although the results shown on the graphs on **Figures 4-1**, **4-2** and **4-3** do indicate differing overall wayside noise levels between the four SCLRS designs, the variances were hard to distinguish audibly roadside. However, an external vibratory response (shaking) of the heavy truck was observed when testing SCLRS S3A, and loud wayside roadside rumble was heard roadside when all vehicles stuck MDT's standard CLRS (Appendix B).

As discussed in **Section 4.1**, for each vehicle and test speed the wayside noise levels of the four SCLRS designs are similar to each other, and one design is not significantly quieter than another. In general, the wayside noise level difference between MDT's standard CLRS and the four SCLRS designs increased with increasing speed for each vehicle type, with the largest difference occurring at 70 mph.

The largest difference between the CLRS and the SCLRS designs occurred for the passenger vehicle, and the smallest difference occurred for the medium truck. The difference appears to be due to how much contact the vehicle's front and rear tires have with the rumble strips. For the passenger vehicle, both the front and rear tires were in contact with the strips. For the medium truck, the front tire was aligned with the space between the two dually rear tires. Therefore, although the medium truck front tire was in contact with the rumble strips during the tests, the rear tires were only partially in contact with the strips. For the heavy truck, the front tire and the outer

rear tires were approximately in alignment (**Appendix A**), and in contact with the strips. Therefore, the inner rear tires on the heavy truck did not contact the strips.

Figure 4-4 on the next page, indicates the measured 1/3-octave band L_{max} spectra for the SCLRS designs are similar for each vehicle type and speed combination, and the SCLRS spectra are similar to the pavement spectra. The comparison of frequency spectra confirms that the noise generated by the four SCLRS designs and the pavement all sound very similar. The prominent peaks for all vehicles in the spectra between 50 Hz and 125 Hz are due to the forcing and second harmonic frequencies of the tires rolling over the 14-inch longitudinal frequency of SCLRS S1 and S3, and the 24-inch longitudinal frequency SCLRS S2 and S3A, which varies by speed (TRB 2017). Although these peaks are pronounced in the spectra, they are lower than the general "hump" in the SCLRS spectra around 800 to 1,000 Hz, which is typical for tire-pavement noise.



Figure 4-4: Measured Average Lmax 1/3-Octave Band Frequency Spectra

4.3 Interior Observations

The purpose of the project was to measure the exterior wayside noise of the standard CLRS and four SCLRS rumble strip designs (Section 1.0). Therefore, interior noise levels inside the vehicles or steering column vibration were not measured. However, in order to help determine the noise and vibratory effectiveness of the differing SCLRS designs, the drivers made qualitative assessments, took notes, and made dash videos of the interior conditions inside the vehicles during the field testing, as listed in Table 4-3 and Appendix B.

Rumble Strip Design	Sneed	Passenger Vehicle	Medium Truck	Heavy Truck	Driver Opinions of Bumble Strip
Design	30 mph	Low rumble	Loud vibrations	Loud vibrations	Loud interior noise
MDT Std	50 mph	Louder and shaking interior	Loud vibrations	Loud vibrations	and vibration levels
CLRS	70 mph	Loud noise and vibrations	Loud vibrations	Loud vibrations	
	30 mph	Steering wheel vibrations,	Very hard to stay on	Quiet and very smooth (i.e.,	Concerned that S1
		Oujeter than 30 mph.	Smoother (i.e., less	Smooth, but more vibration	drivers to overcorrect
SCLRS S1 14" LF,	50 mph	steering wheel vibrations, pushed car off rumble strip	vibration) than 30 mph	than 30 mph	when coming into contact with strip,
12" wide	70 mph	Quieter than 30 mph, louder than 50 mph	Very rough and pushed truck off rumble strip	Louder than 30 and 50 mph, but pushed and pulled truck off rumble strip	since vehicles were "pushed" off strip.
	30 mph	Quietest interior noise and vibration levels	Smooth and quiet	Little vibration and noise	Concerned that S2 would not alert or
SCLRS SZ	50 mph	Very quiet	Very little vibration	Little vibration and noise	rouse a driver of all
12" wide	70 mph	Same as 50 mph, lower frequency than S1	Very little vibration	Little vibration and noise	vehicle types effectively at all speeds.
SCLRS S3 14" LF,	30 mph	Noise and vibration in front end of vehicle, and louder when on tapered edge	Smooth and quiet, but a little more vibration than S2	Very quiet	Design S3 appeared ineffective for a heavy truck, and may
14" wide-	50 mph	Same as 30 mph	Same as 30 mph	Hardly noticeable noise or vibration	not alert or rouse a driver effectively.
tapered	70 mph	Same as 30 mph	Same as 30 mph	Hardly noticeable noise or vibration	
SCLRS S3A	30 mph	Lots of noise and vibration	Good sound and vibrations	Better than S1, S2 and S3, i.e., more noticeable noise and vibration inside truck	Favorite SCLRS tested by drivers. Effective noise and vibration
24" LF, 14"	50 mph	Quieter and less vibration than 30 mph	Quieter than 30 mph	Same as 30 mph	for all vehicle types and at all speeds.
wide- tapered	70 mph	Good noise and vibration, louder than 50 mph, less than 30 mph.	Louder sound and vibrations than 30 & 50 mph	Same as 30 mph	

Table 4-3: Driver Interior Observations Noted during Testing

4.4 Sources of Error and Variables

There were several potential sources of error and variables that could have affected the measurement results, as listed below.

- Diesel engine noise from the medium dually truck may have influenced some of the measurement results.
- Condition and age of the tires on the vehicles at the time of the measurements. Different tread patterns and depth of tread patterns may produce different results for the same types of vehicles.
- Different tire sizes. Both 12-inch wide and 14-inch wide-tapered SCLRS designs were tested, with depths ranging from 1/8 to ½-inches deep (Section 1.0). Therefore, width of the tires tested (9 to 10.8 inches) and positioning on the vehicle (Section 4.2) determines the amount of tire in contact with the rumble strip, versus the pavement, concurrently.
- Different pavement types will produce varying noise level results based on wear, age, size of chipseal aggregate, or smoother pavement. Type 1 chipseal, 3/8-inch aggregate, overlayed in 2011, was tested for this project, and the SCLRS were milled in 2018 (MDT 2019).

5.0 LITERATURE REVIEW

Many States have different standard rumble strip configurations, and are evaluating the effectiveness of varying designs of sinusoidal rumble strips. Numerous longitudinal frequencies (12 to 24 inches), widths (8 to 16 inches) and depths (1/8 to 1/2 inches) have been tested on varying pavements, speeds, and using different vehicle types. In general, shorter longitudinal frequency designs (12 to 16 inches) have been more effective at shallower depths (5/16 inches or less), and tapered width patterns have been more effective than straight edge patterns (Caltrans 2018a). Because of the many sinusoidal patterns tested, it is challenging to correlate the data results and conclusions among the studies, and to date, the optimal design for all vehicle types has not been determined. However, similar to the findings of this project, the studies reported lower wayside noise levels in all vehicle types for sinusoidal designs, and a greater interior noise and vibration response in passenger vehicles than heavy trucks (Caltrans 2018a, Mathew 2018, MNDOT 2016, WSDOT 2018).

The National Cooperative Highway Research Program (NCHRP) recommends that centerline rumble strips should be designed to produce interior sound level differences (above background) of 10 to 15 dBA inside the passenger compartment in rural areas, and 6 to 12 dBA near residential or urban areas (NCHRP 2009). Chipsealed pavements produce higher background noise levels, and therefore, effective rumble strip designs in Montana need to produce higher absolute interior sound levels, which were not measured for this project.

6.0 CONCLUSIONS

This wayside noise study helped determine whether or not the four SCLRS designs installed on MT-39 reduced exterior noise compared to MDT's standard CLRS. For the passenger vehicle, medium truck and heavy truck tested at 30, 50 and 70 mph, the wayside noise levels of the four SCLRS designs are similar to each other, and one design is not significantly quieter than another. The wayside noise levels of the four SCLRS designs are also similar to the chipsealed pavement (baseline) at each speed, for each vehicle type (**Figures 4-1, 4-2 and 4-3**).

The wayside noise level difference between MDT's standard CLRS and the four SCLRS designs increase with increasing speed for each vehicle type, with the largest difference occurring at 70 mph. The wayside noise difference between MDT's standard CLRS and the four SCLRS designs are shown graphically in **Figures 6-1**, **6-2** and **6-3**.



Figure 6-1: Difference between CLRS and SCLRS Noise Levels—Passenger Vehicle

1.8 to 4.4 dBA quieter at 30 mph (i.e., a barely to clearly noticeable reduction)8.2 to 9.2 dBA quieter at 50 mph (i.e., a clearly noticeable reduction to half as loud)12.8 to 13.4 dBA quieter at 70 mph, which is typically perceived as half as loud (Egan 1988)



Figure 6-2: Difference between CLRS and SCLRS Noise Levels—Medium Truck

Within -0.8 to 0 dBA at 30 mph (i.e., imperceptible) 2.4 to 4.2 dBA quieter at 50 mph (i.e., a barely noticeable reduction) 5.1 to 6.1 dBA quieter at 70 mph, (i.e., a clearly noticeable reduction) (Egan 1988)





Within -0.5 to 3.2 dBA at 30 mph (i.e., imperceptible)

1.8 to 4.6 dBA quieter at 50 mph (i.e., a barely noticeable reduction)

8.4 to 9.5 dBA quieter at 70 mph (i.e., a clearly noticeable reduction to half as loud) (Egan 1988)

The interior noise levels inside the vehicles or steering column vibration were not measured for this project. However, as listed in **Table 4-3**, for design SCLRS S3A (i.e., 24-inch longitudinal frequency, 14-inch wide tapered) the drivers noticed the most interior noise and vibration in all vehicle types at all speeds of the SCLRS designs. MDT's standard CLRS also provided considerable interior noise and vibration in all vehicle types, but significantly louder wayside noise levels at faster speeds than all the SCLRS designs.

7.0 **RECOMMENDATIONS**

Some interior response from all the SCLRS designs was noted in the passenger vehicle, but the CLRS and SCLRS S3A provided the most interior response in all the tested vehicles (**Table 4-3**). Before MDT standardizes a SCLRS design for use on Montana's roadways, interior noise and vibration (i.e., seat track and steering column) should be tested to comply with NCHRP guidelines (NCHRP 2009). BSA also recommends testing a small passenger vehicle with narrower tires (less than 9 inches), to determine the internal noise, vibration and variability responses of a small car on the MT-39 SCLRS designs.

The Federal Highway Administration (FHWA 2015) published guidance for rumble strip setback distances for two-lane roadways. Studies cited determined that when standard rumble strips end approximately 650 feet (direct distance) prior to a noise-sensitive receptor (i.e., residence) or urban area the noise impacts are "tolerable", and within 1,640 feet the noise generated from standard strips is "negligible". MDT should monitor current guidance and consider appropriate setback distances when terminating standard rumble strips in residential or urban areas and/or replacing with sinusoidal strips.

MDT should monitor/observe the four SCLRS designs during the winter months to determine if water pooling/ice collects in the SCLRS troughs, which may be a safety issue. MDT should also continue to monitor the durability of the SCLRS and striping over the years for degradation due to snow removal and/or normal wearing.

The California Department of Transportation (Caltrans 2018b) has extensively studied "mumble" strips (aka sinusoidal rumble strips), and recommends the following key design parameters of SCLRS for MDT's consideration if installed in Montana:

- Provide lower roadside noise levels.
- Maintain or increase interior sound and vibration levels.
- Cause minimal disturbance to vehicle dynamics.
- Be bicycle friendly design considerations for safe bicycle navigation on shoulder sinusoidal rumble strips (e.g., adequate riding space—4 feet from edge of pavement, and gaps for exiting and entering bicyclists) (TRB 2017).
- Fit within the roadway cross-section, limit depth of material removal, be cost effective, and provide ease of construction (Caltrans 2018b).

8.0 **REFERENCES**

California Department of Transportation (Caltrans). 2018a. Design and Acoustic Evaluation of Optimal Sinusoidal Mumble Strips versus Conventional Rumble Strips. April.

California Department of Transportation (Caltrans). 2018b. *Sound Advice for Mitigating Roadside Rumble Strip Noise Levels*. Presentation by Bruce Rymer/Caltrans and Dave Buehler/ICF.

Egan, M. 1988. Architectural Acoustics. McGraw-Hill, Inc., New York, New York.

Federal Highway Administration (FHWA). 2015. Rumble Strip Implementation Guide: Addressing Noise Issues on Two-Lane Roadways.

Mathew, J. K., Balmos, A. D., Plattner, D., Wells, T., Krogmeier, J. V., & Bullock, D. M. (2018). *Assessment of Alternative Sinusoidal Rumble Stripe Construction* (Joint Transportation Research Program Publication No. FHWA/IN/JTRP-2018/05). West Lafayette, IN: Purdue University. https://doi.org/10.5703/1288284316648

Minnesota Department of Transportation (MNDOT). 2016. Sinusoidal Rumble Strip Design Optimization Study. Final Report. June.

Montana Department of Transportation (MDT). 2019. Experimental Projects Construction Report, *Sinusoidal Centerline Rumble Strip (SCLRS) Evaluation*. April.

National Cooperative Highway Research Program (NCHRP). 2009. NCHRP Report 641, *Guidance for the Design and Application of Shoulder and Centerline Rumble Strips*. MTU TTAP ID# 2233.

Transportation Research Board (TRB). 2017. Webinar Program. *Highway Rumble Strips: Approaches to Balancing Public Safety and Community Noise*. Presented by Judy Rochat, Cathy Satterfield, Bruce Rhymer and Paul Donavan. March 28.

Washington State Department of Transportation (WSDOT). 2018. Evaluation of New Rumble Strip Designs to Reduce Roadside Noise and Promote Safety. May.



Microphone at each measurement location was 5 ft above the road surface, and between 8 and 9.5 feet above the ground surface.

Big Sky Acoustics

FIGURE 1

Rumble Strip Wayside Noise Study Rumble Strip Sections and Noise Level Measurement Locations

Appendix A

Photolog

Appendix A: Photolog



Appendix A: Photolog



Appendix **B**

Field Notes

19134 BSA Project #: Project: Rombe Svile - MBT Date: 7/26/16 -Thes Name: Response: SLM: NA S/N: 1 NA S/N: Calibrator: Location: NB/5B MT-39 May 160' Set up After Meas: NA Before Meas: Calibration: End Time: Start Time: NA Weather(Conditions: NIX level both pides of road, plope to borrow pit, this height adj to Notes/observations (audible noises, line of sight map, etc.), the state of the pavement of the state of the Ground Conditions/topography: 45,497 2, -106. 1596 GPS 50 45. 1973, -106.6372 46,000, -106,6599 mic height: Results: (SPL's, dominant source(s), etc.) 46.0001, -106.6714 reactions of 7

(construed)

FIDIECI.		BSA Project #
Name:		Date
SLM:	S/NI-	Pesporso:
Calibrator	S/N-	Incopulse.
Location:	5/N.	
Calibration:	Before Meas:	After Meas:
Start Time:	End Time:	
Weather Conditions:		
Ground Conditions/topograph	у:	
	Star W. 0067	-106.665) -106.665)
53)	(16) 73-63 46, 011 521 73-63 46, 011 521 73-63 46, 011 521 73-63 46, 011	51-106.66591 N->
Results: (SPL's, dominant sou	urce(s), etc.)	N6-0135, -126.1705

Big Sky Acoustics, LLC Field Noise Level Measurement Data Form

BSA Project #: 19134 Project: Proper strip Date: 7/30/19 - Wed Name: PAL 30 SLM: 40#1 1# mict prim Response: A.f. W/4 S/N: Calibrator: Lp S/N: l ocation: Standind CURS After Meas: Before Meas: Calibration: 0724 End Time: 08/9 Start Time: Weather Conditions: See helows Ground Conditions/topography: Ground Conditions/topography: <u>livel</u>, <u>slope</u> to borrow pit, <u>gras/weeds</u> Notes/observations (audible noises, line of sight, map, etc.) Mill - NB 4T-073101.004 723 from her power glant in titl, from the power glant in title from the power gla HT- 073762.007 (8 5H-50 HT-00) 076406 - Londy har rundle 701 MT- 673812.008 MT 602 072539 - more mighte 4.9 MT- 673812.008 CY 603 072638 - some rudle - 655 (M 695550-.009) HT- 95816 OL 08 Sth-NB HT0747 MT- 95974 617 08 Sth-NB HT0747 HT- 05816 OL 5mg 010 .DII Car- dato off Conotigiz 012 NY Results: (SPL's, dominant source(s), etc.) HT .013 Olath-9 MT - OM Ing -015

Stacues of

Project:		BSA Project #:		
Name:		Date:		
SLM:	S/N: Response:			
Calibrator:	S/N:			
Location: 57d CLRS	5			
Calibration:	Before Meas:	After Meas:		
Start Time:	End Time:			
Weather Conditions:				
Ground Conditions/topogra	aphy:			
Notes/observations (audib	le noises, line of sight, map, etc.)			
Stal Toingh	KSHA-NB	- 56md 4 bird + 19p1 HT022 87 MT .023 82 CM .024 87		
		N->		
	HT .025 OPSHI- 50	HT ON SE		
	att old	MT 170 55		
	n . /			
	(m -out	Cim , 02 85		
Results: (SPL's, dominant	source(s), etc.)			

SHELRS 2 of 2

19134 BSA Project #: Project: Rmal Stin Date: 7/30/14 Name: Response: S/N: SI M S/N Calibrator: Location: 51 SCLRS After Meas: Before Meas: Calibration: 0844 End Time: Start Time: Weather Conditions: see helow Ground Conditions/topography: level, slope to bourow pit, grass/weeds Notes/observations (audible noises, line of sight, map, etc.) 57 - thirt make HT. 028 HT- 6855142 :07 093- MB MT . 029 mr - 030 insits Nt 9-51-58 HT - 031 - 20572 MT- 032 - 20372 Chy- 633 - fillt rm Results: (SPL's, dominant source(s), etc.) 70, 68/6 com weather Page

Project:		BSA Pro	ject #:
Name:	95. -	Date:	
SLM:	S/N:	Respons	se:
Calibrator:	S/N:		
Location: SCURS 51			
Calibration:	Before Meas:	After Me	as:
Start Time:	End Time:		
Weather Conditions:			
Ground Conditions/topography:	308.		
Notes/observations (audible nois	es, line of sight, map, etc.)		
(3)		11	
mark		HT - 040	
March	QSI-NB	MT ON	
		CM - 042	
	20		
	and An		
			11-3
	$\frac{1}{1} \sum_{i=1}^{n} \frac{1}{i} \sum_{j=1}^{n} \frac{1}$		N-1
	the tab		
no	HT- 243 BS1-51	45-037	- inthemale not n
Angine, -	AT- OWN	TIFECTI	
-first mobile	- 18	MT 038	- ansthe
- Costmil	, cr 017	14 136	- new little mile
-(-1(-1)		107-071	
Results: (SPL's, dominant sourc	e(s), etc.)		
Togis - 821 F. 50% (Am	-3minDi weather		
City art art and	17		

SPage 2 of 3

Project: Proble Strip BSA Project #: Date: 7/30/19 Name: SLM: S/N: Response: Calibrator: S/N: Location: SCIRS 51 Calibration: Before Meas: After Meas: Start Time: End Time: Weather Conditions: Ground Conditions/topography: Notes/observations (audible noises, line of sight, map, etc.) HT 052 m? 45 - MT 053 m? 45 - and 054 74 Yes TO SI-ND HT ONC - maring truck around MT ONT - mgine mostly and out - mynot he ten on strip 74 N-3 By-50 HT-050 - mgine ar 051 - on it that in - finit multi-- thing pushing whichs around - 'hud to stay on strip" 1.1 Results: (SPL's, dominant source(s), etc.) JAN5 - 827, 55% RH, Uhm) weather

SI Page 3 of B

Ruble Stip Project: BSA Project #: 19/34 Name: Date: 7/30/19 SLM: S/N: Response: Calibrator: S/N: Location: SILRS 52 Calibration: Before Meas: After Meas: V Start Time: 1103 End Time: 1142 Weather Conditions: see blow Ground Conditions/topography: Devel, plope to borrow pit, tall grasses / weeds Notes/observations (audible noises, line of sight, map, etc.) 52 HT-035 - no visible (200) 40 MT-056 - no number (108) 60 Car-057 - no paulok 118517 62 HT-MT-OR-NB Ht - 058 (M) 72 MT - 059 (M) 47 car , obe loss of 1-3 $\frac{1}{100} + \frac{1}{100} + \frac{1}$ Results: (SPL's, dominant source(s), etc.) 1100 - 870 F, 51/. RH, chm

52 Page of 3

Project: Romble		BSA Project #:
Name:		Date: 7/3019
SLM:	S/N:	Response:
Calibrator:	S/N:	
Location: SCLRS SZ		
Calibration:	Before Meas:	After Meas:
Start Time:	End Time:	
Weather Conditions:		
Ground Conditions/topography		
Notes/observations (audible no	ises, line of sight, map, etc.)	
C.F.		
	×	NS
-	1	
HT: OGY (NB)	- 667(46) 67	D (MB)
m7: 0(5 (ND)	- 069(56) 07	(195)
put the	m(G. (3B) 077	- (NB)
ar 1040 (WY	- Uvilliy	
Results: (SPL's, dominant sou	rce(s), etc.)	
	i.	

52 Page 2 ofB

Project: Rmlbr			BSA Project #:	
Name:			Date:	
SLM:	S/N:		Response:	
Calibrator:	S/N:			
Location: SCLRS	52			
Calibration:	Before Me	eas:	After Meas:	
Start Time:	End Time	1		
Weather Conditions:				
Ground Conditions/topograp	hy:			
Notes/observations (audible	noises, line of sight, map, e	etc.)		
冠	- ARSI	2-108		
Tomp				
01 -				
				\xrightarrow{N}
15- 073 (NB)	- 096 (55)) 079 (M)		
mT- 674 (MD)	- 1377 (3F)) 050 (WB)		
in the late	1	DS (48))	
an- 673 (10)	- 070 cm)	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		
- my rvalle	for my which.			
ε	v			
Results: (SPL's, dominant so	ource(s), etc.)			

52 Page 3 of 3

Project: Rimble		BSA Project #: 19134
Name:		Date: 7/30/19
SLM:	S/N:	Response:
Calibrator:	S/N:	
Location: SCLRSS	3	
Calibration:	Before Meas:	After Meas:
Start Time: 1206	End Time: /244	1
Weather Conditions: See below		
Ground Conditions/topography:	to borrow pit, for	Il gasses/weeds
Notes/observations (audible nois	es, line of sight, map, etc.) $\bigcirc 53 - N^{\beta}$	
30mp -		A1
		~~~>
HT- 052-(ms)	- 585 - 088	
MT- 683/10	- 056 - 089	
(m- 084 (M)	- 087 - 690 (Rp	it nucker)
- no smalle	for any whicky	
	V	
Results: (SPL's, dominant source	e(s), etc.)	

53 Page Tof 3

Project: Rombe thil		BSA Project #:	
Name:		Date: 7/30/19	
SLM:	S/N:	Response:	
Calibrator:	S/N:		
Location: SCLRS	53		
Calibration:	Before Meas:	After Meas:	
Start Time:	End Time:		
Weather Conditions:			
Bround Conditions/topograph	y:		
Notes/observations (audible n	oises, line of sight, map, etc.)		
163)	N 53-14		
(amp)	C4		
0 30 0			
		V	
	a. (.) (67		
HT - 041 la	(B) - O(4)(MP) - O(4)		
MT - 017-1	NB - 095 (mb) - 699		
lar- 593 (	NB) - (MGL (MA) SGA		
- no m	ntele		
Results: (SPL's, dominant sou	Irce(s), etc.)		
1010 - 20	1 3.10		
1215-92F, 41/.BH	Com - July		

53 2 3 3

Project: Rumble		BSA Project #:
Name:		Date=7/30/19
SLM:	S/N:	Response:
Calibrator:	S/N:	
Location: SCUR	\$ 53	
Calibration:	Before Meas:	After Meas:
Start Time:	End Time:	
Ground Conditions/topography		
Notes/observations (audible no	ises, line of sight, map, etc.)	
33 ADmyb	@ 53 - M9	
		$N \rightarrow$
	24	
HT- 100 (N	10) - 103 - 106	
mt - 101 (m Com - 102 (m	m - 109 - 107 m - 105 - 109 - 107	Fint rumble
- no rough	a forwhidey	
~		
Results: (SPL's, dominant sour	ce(s), etc.)	

53 Page 3 of B

		BSA Project #:
Name: GC		Date: 7/30/19
SLM:	S/N:	Response:
Calibrator:	S/N:	
-ocation: SCLRS S	53A	
Calibration:	Before Meas:	After Meas:
Start Time: 1301	End Time: /335	
Ground Conditions/topography:	>	
Votes/observations (audible noise	es, line of sight, map, etc.)	N->
HT- 109-1600 MT- 110-	hr; truck shiking - 112 - 113	-(m how rattle (thint) - 115 - 116
HT- 109-1600 MT- 110- Car- 111- 1 - "Campa	br; truck shiking - 12 - 113 not much "rumik" - 114 el vitration "monetum others"	-(m how rattle (thint) - 115 - 116 - 117
HT- 109-1600 MT- 110- Car= 111- 1 -112mmfd	br; truck shiking - 12 - 113 20t much "monste" - 114 el vitration "monstrum otrurs"	-(m how rattle (fint) - 115 - 116 - 117



		BSA Project #:
Name:		Date: 7/30/19
SLM:	S/N:	Response:
Calibrator:	S/N:	
Location: SCLRS S3	A	
Calibration:	Before Meas:	After Meas:
Start Time:	End Time:	
Weather Conditions:		
Ground Conditions/topography:		
Notes/observations (audible noises,	line of sight, map, etc.)	
37/4 Bo-mgh	0 <b>33</b> 4 - NB	
		$\sim \rightarrow$
HT - 114	- (z.) -	(24
MT_ 119	- 122 =	175
A state of the Al	(1-0) 22	
Results: (SPL's, dominant source(s),	etc.)	

Project: Runny		BSA Projec	ct #:
Name:		Date:7/3	119
SLM:	S/N:	Response:	
Calibrator:	S/N:		
SCLRS 53	A		
Calibration:	Before Meas:	After Meas	í.
Start Time:	End Time:		
Neather Conditions:			
Ground Conditions/topography:			
Notes/observations (audible noise	s, line of sight, map, etc.)		
57A)	(8)53A- MB		
Aomp			
			N->
HT = 127 - Ch	n 2 this "bunghing" - 130	- 133	
MT - 129	- 131 -	- 134	
Cor - 129	- 132 -	- 175	
- no "m	ndohe v	1.17	
*	u.		
- priver ferrorit	レヨ		
esults: (SPL's, dominant source(s	s), etc.)		
1220 0	7 18		
1 m TOF, Mar Oft, An	m-2mgh-7		

Page 3 of 3

Big Sky Acoustics, LLC Field Noise Level Measurement Data Form

Project: Rmak Strip 19134 BSA Project #: Name: Date: 7/30/17 SLM: S/N: Response: Calibrator: S/N: Location: 33A-NB Chipseal Pavement only Calibration: Before Meas: After Meas: End Time: 1410 Start Time: Weather Conditions: pane as 53A Ground Conditions/topography: Dame as 53/ Notes/observations (audible noises, line of sight, map, etc.) prement \$ 100 rouble string CASA- NB No 30 mgb HT - 136 (MB) - 139 (SB) - 142(MB) MT - 137 (MB) - 140 (SB) - 143 (NB) Cm - 138 (mB) - (11 (50) - 144 (MB) Results: (SPL's, dominant source(s), etc.) HT - 154(NB) - 157(SB) - 160 (NB) MT - 155 (NB) - 158(BD) - 161 (NB) 1m- 156(NB) - 1596B)cd die: 1911 - 114.1/18 Chipseal Pavement of

### Rumble Strip Wayside Noise Study Work Plan

### **Big Sky Acoustics**

	RI	umble	Strip V	Vaysid	e Nois	e Stud	y Field	lwork	Driv	Totes	Date: 7/30/19
Rumble			Car	)	м	edium Ti	ruck		leavy Tru	ick	Passinger Vehicle
Strip Design	Speed	Time/	Time/	Time/	Time/	Time/	Time/	Time/	Time/	Time/	4 Runner
a caigi	30 mph	0847	0855	0900	0846	0857	Lmax 08.59	U844	0853	L _{max} 0858	Notes & Met Data hand to play on ship steaming wheed vib
SCLRS S1	50 mph	0907	0912	69.19	0906	0911	0918	0905	0910	0916	quiting them 30mp
	70 mph	6929	0941	0954	0928	0940	0951	0929	0939	0950	queter the Strip
	30 mph	1105	1109	7177	1104	1108	1111	1103	1107	1110	amietost yetin
SCLRS S2	50 mph	1115	1116	1120	1115	1116	1120	1134	1117	1119	iley quit
	70 mph	1132	.1137	1142	[13(	1136	1142	114t	1135	i130	lower freg than
	30 mph	1207	1211	1214	12:06	1211	1214	1206	1210	12/3	more wase affer
CLRS S3	50 mph	1219	1224	1228	1219	1224	1228	1218	1223	1227	poise & Vib in fee
	70 mph	1232	12.38	1244	1232	1237	1243	1231	1236	1242	than with off of
	30 mph	1302	1305	1308	1301	1305	1308	1301	1304	1307	lots of vibratio
CLRS S3A	50 mph	13	1317	1320	13	1317	1317 1320	13毫	1316	1319	quieter & less ci.
	70 mph	1327	/331	/335	1327	1331	1335	1326	1330	1334	good noise & vib loads, than 50 mp
	30 mph	0126	0732	0738	0725	0731	D737	07对	0730	0736	downently interor
td CLRS	50 mph	0748	0753	0759 V	0747	0752	0758	0745	0750	0757	loudar, shaking not
	70 mph	0805 V	0811 V	0819	0804	0810	0817 19107	0802	0809	0816	nock & Noll Deby
The s	30 mg	13:5	1347	1349	1345	1347	anned	1344	1346	1348	dy procements
veniera	50 A	1351	353	355	1350	1352 Page 3 c	1354	1350	1352	1354	to all stri
4	1/m h	1400	1404	1408	1400	1403	1408	1359	1403	1407	

### Rumble Strip Wayside Noise Study Work Plan

+

-

### **Big Sky Acoustics**

	Ru	mble S	Strip W	Vaysid	e Nois	work	Dri	ver Intes	Date: 7/30/19		
Rumble		Car			M	Medium Truck			leavy Tru	ck	Modium Truck Equipment: 2007 July
Strip Design	Speed	Time/ L _{max}	Time/ L _{max}	Time/ L _{max}	Time/ L _{max}	Time/	Time/ Lmax	Time/	Time/	Time/	Ram Dually 3500 Notes & Met Data
	30 mph				X	X	X				Very hard to
SCLRS S1	50 mph				X	X	X				Smooth
	70 mph				X	X	X				Very Rough Dished Fairt
SCLRS S2	30 mph				X	X	Х				Smooth /quici
	50 mph				X	X	X				very little vibration
12-1	70 mph				X	X	X				4
0.44	30 mph				X	X	X				Smooth a little
SCLRS S3	50 mph				X	X	X				than 52
	70 mph				Х	$\times$	X				for the second of the second o
	30 mph				X	X	X				Good Libration
SCLRS S3A	50 mph				$\times$	Х	X				more quiet than Smoother than
	70 mph				$\times$	X	X				Better than # K
	30 mph				X	X	X				Loud Ubrations
Std CLRS	50 mph				X	X	X				
	70 mph				X	X	X				

19

### Rumble Strip Wayside Noise Study Work Plan

### **Big Sky Acoustics**

	Ru	mble S	Strip W	/ayside	e Nois	e Stud	y Field	work	Driv	fes	Date: 7/30/19	
Pumbla		Car			M	edium Tr	uck	H	eavy Tru		Heavy Truck Equipment: 2000 Volve	999
Strip Design	Speed	Time/ L _{max}	Time/ Lmax	Time/ L _{max}	Time/ Lmax	Truck Tractor Notes & Met Data 30 (which very smooth)						
	30 mph							1	1	~	consulta	
SCLRS S1	50 mph							V	~	V	hear numble strips better than 30 mph	
	70 mph							~	~	~	numble even louding	_
SCLRS S2	30 mph							~	r	~	little vitration/	
	50 mph							~	~	1	HALE VIbration	
	70 mph				7			~	~	1	11the vibrition ] noise	
	30 mph				- fY (	1		1	V	~	very quilet	
SCLRS S3	50 mph							V	~	1	Hardly noticable)	
	70 mph				1			V	~	~		_
	30 mph							~	V	V	20ther thin 51/52/253	
SCLRS S3A	50 mph		-					V	~	~	terms of rundle st	rips
	70 mph						L	V	~	V	being more noticable trutte for noise and vibration	histole
	30 mph							r	~	~		
Std CLRS	50 mph				3			V	~	~		
	70 mph							V	~	1		

ł

20

.